



ASX Announcement

2<sup>nd</sup> June 2023

## Large Gold System Confirmed at Fortitude North Lake Carey Gold Project

### HIGHLIGHTS

- All assay results from the 2023 RC drill program of 20 holes focussed in the north of Fortitude North have now been received
- Seven of the top twelve intercepts at Fortitude North have come from the 2023 program (hole ids are prefixed with the year drilled):
  - **25m @ 3.3g/t Au** from 147m (23FNRC006)
  - **14m @ 3.4g/t Au** from 113m, and;
  - **35m @ 3.0g/t Au** from 150m (23FNRC016)
  - **19m @ 3.8g/t Au** from 100m (23FNRC011)
  - **11m @ 3.8g/t Au** from 108m (23FNRC017)
  - **11m @ 4.2g/t Au** from 130m (23FNRC007)
  - **12m @ 3.4g/t Au** from 143m (23FNRC022)
  - **47m @ 2.55g/t Au** from 42m (18FNAC071)
  - **4.0m @ 13.6g/t Au** from 79m (20FNDD002)
  - **3.4m @ 12.3g/t Au** from 64m (20FNDD003)
  - **10.3m @ 3.5g/t Au** from 124.6m (20FNDD004)
  - **9.6m @ 3.3g/t Au** from 120.8m (22FNDD009)
- The width and grade of these intersections are confirmation that Matsa has discovered a major gold mineralised system which remains open in all directions and additional drilling could further add significantly to the size of the defined mineralisation
- Key geological observations have established that there are multiple stages and styles of mineralisation, which invites comparisons to the world class 12M oz Sunrise Dam gold deposit located just 23km to the north within the same complex regional structure and geological setting
- The mineralisation at Fortitude North has now been defined by drilling over a strike length of 1.7km and has also been extended to the east by 70m to 250m across strike in the northern area

### CORPORATE SUMMARY

#### Executive Chairman

Paul Poli

#### Directors

Pascal Blampain

Andrew Chapman

#### Shares on Issue

412.07 million

#### Unlisted Options

27.15 million @ \$0.08 - \$0.21

#### Top 20 shareholders

Hold 59.16%

#### Share Price on 1<sup>st</sup> June 2023

3.6 cents

#### Market Capitalisation

A\$14.83 million

Matsa Resources Limited (“Matsa”, “Company”) is pleased to advise excellent results from reverse circulation (RC) drilling at Fortitude North, Lake Carey (Figures 1 to 4). The drilling has now extended the Fortitude North discovery by 200m to the north resulting in a strike extent of 1.7km which remains open in both directions along strike. In addition, the drilling has extended mineralisation down dip to the east by 70m for a total width of some 250m across strike. The new 2023 drilling has added significantly to the potential size and scale of Fortitude North.

Of the 20 holes drilled there were:

- **10 intercepts above 25 gram metres**
- **3 intercepts above 50 gram metres**
- **1 intercept above 100 gram metres, and**
- **13 intercepts greater than 10m thick**

Multiple lodes were intersected within a number of holes whose results are highlighted in Table 1 below:

| holeid    | Comment / Assays (Au @1g/t cutoff)                                    | Intercept (m) | Grade (Au g/t) | Gram x meter | Intercept (m) | Grade (Au g/t) | Gram x meter |
|-----------|---|---------------|----------------|--------------|---------------|----------------|--------------|
| 23FNRC006 | <b>25m @ 3.3g/t Au</b> from 147m                                      | 25            | 3.3            | <b>83</b>    |               |                |              |
| 23FNRC007 | <b>11m @ 4.2g/t Au</b> from 130m and 6m @ 2.1g/t Au from 148m         | 11            | 4.2            | <b>46</b>    | 6             | 2.1            | <b>13</b>    |
| 23FNRC008 | 1m @ 1.1g/t Au from 99m   | 1             | 1.1            | 1            |               |                |              |
| 23FNRC009 | 2m @ 1.5g/t Au from 115m  | 2             | 1.5            | 3            |               |                |              |
| 23FNRC010 | <b>14m @ 2.9g/t Au</b> from 130m and 30m @ 1.3g/t Au from 160m        | 14            | 2.9            | <b>41</b>    | 30            | 1.3            | <b>39</b>    |
| 23FNRC011 | <b>19m @ 3.8g/t Au</b> from 100m and 3m @ 2.1g/t Au from 134m         | 19            | 3.8            | <b>72</b>    | 3             | 2.1            | 6            |
| 23FNRC012 | <b>16m @ 1.4g/t Au</b> from 88m and 4m @ 1.8g/t Au from 124m          | 16            | 1.4            | <b>22</b>    | 4             | 1.8            | 7            |
| 23FNRC013 | 4m @ 3.3g/t Au from 110m  | 4             | 3.3            | <b>13</b>    |               |                |              |
| 23FNRC014 | 11m @ 1.2g/t Au from 67m and 2m @ 1.6g/t Au from 105m                 | 11            | 1.2            | <b>13</b>    | 2             | 1.6            | 3            |
| 23FNRC015 | <b>7m @ 2.1g/t Au</b> from 119m                                       | 7             | 2.1            | <b>15</b>    |               |                |              |
| 23FNRC016 | <b>14m @ 3.4g/t Au</b> from 113m and <b>35m @ 3.0g/t Au</b> from 150m | 14            | 3.4            | <b>48</b>    | 35            | 3              | <b>105</b>   |
| 23FNRC017 | <b>11m @ 3.8g/t Au</b> from 108m                                      | 11            | 3.8            | <b>42</b>    |               |                |              |
| 23FNRC018 | <b>21m @ 1.7g/t Au</b> from 120m                                      | 21            | 1.7            | <b>36</b>    |               |                |              |
| 23FNRC019 | 2m @ 1.5g/t Au from 135m  | 2             | 1.5            | 3            |               |                |              |
| 23FNRC020 | NSA (< 1g/t)  | 1             | 1.0            | 1            |               |                |              |
| 23FNRC021 | * NSA (< 1g/t)  | 3             | 0.3            | 1            |               |                |              |
| 23FNRC022 | * <b>12m @ 3.4g/t Au</b> from 143m                                    | 12            | 3.4            | <b>41</b>    |               |                |              |
| 23FNRC023 | * No lode logged  | 3             | 0.3            | 1            |               |                |              |
| 23FNRC024 | * 1m @ 2.4g/t Au from 164m  | 1             | 2.4            | 2            |               |                |              |
| 23FNRC025 | * <b>17m @ 0.9g/t Au</b> from 121m                                    | 17            | 0.9            | <b>15</b>    |               |                |              |

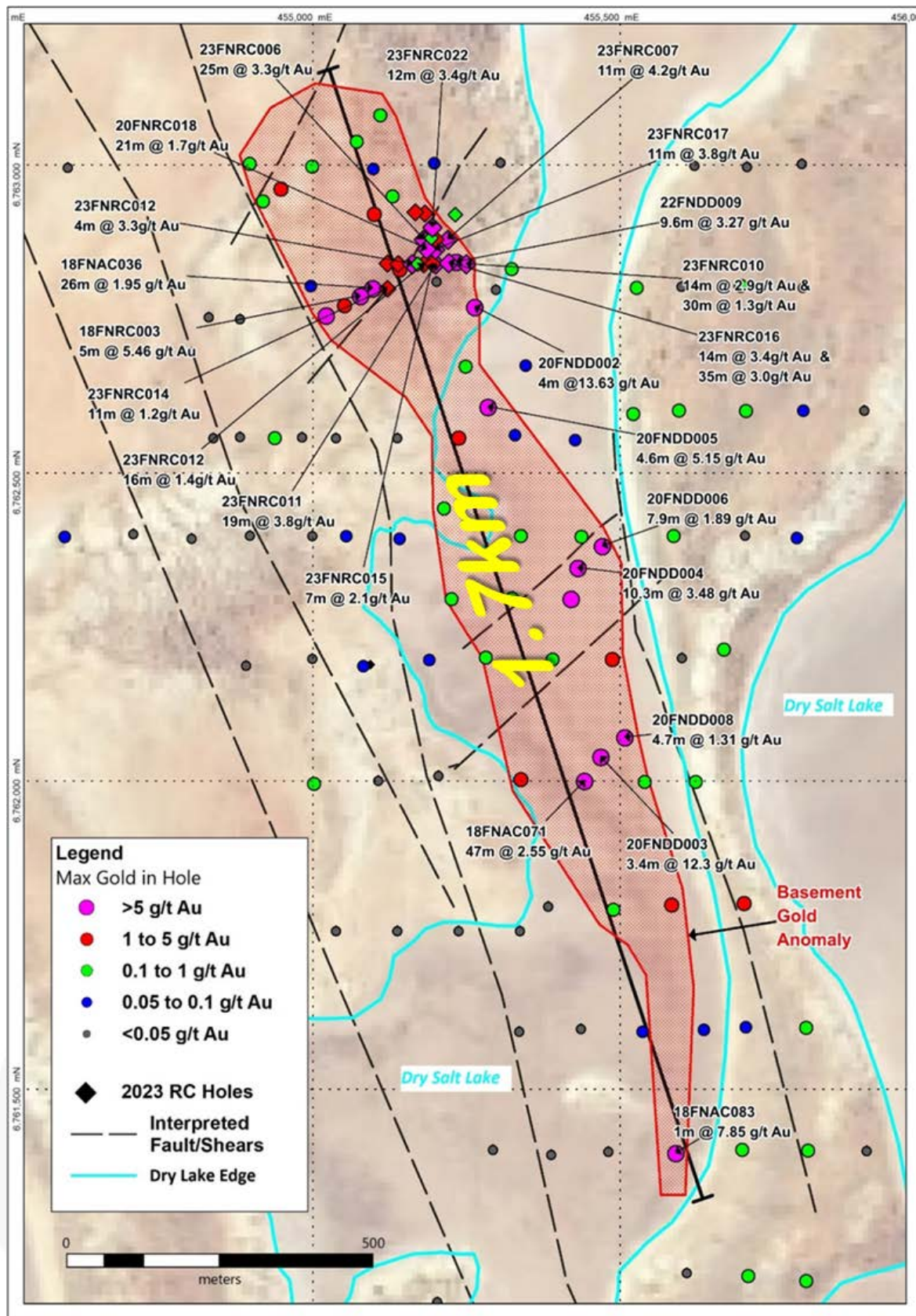
**Table 1: Summary of significant 2023 drilling results (expressed as grade times thickness)**

\*Denotes new results

Drilling continues to extend the bedrock mineralisation at Fortitude North towards the eastern and northern directions and at depth. Mineralised intersections continue to display excellent downhole thicknesses and good continuity. All drilling results are presented on long section (Figure 2) that highlights interpreted high grade shoot geometry. Drill hole section 6762840N (Figure 3) displays the recent results from holes 23FNRC015 and 23FNRC016 extending the known mineralisation approximately 70 metres towards the east with improved grades and thicknesses.

Mineralisation occurs within intensely deformed and altered basalt and dolerite containing minor interflow sedimentary intercalations and late stage felsic porphyry intrusions. The combination of multiple, thick and high grade mineralised intersections demonstrates the presence of a large hydrothermal gold system and supports Matsa’s belief that, with further drilling, Fortitude North will be defined as a major gold deposit.

A summary of all the drilling program can be found in Table 1 and Tables 3 & 4 of Appendix 1. JORC Tables can be found in Appendix 2.



**Figure 1: Summary of Fortitude North drilling updated with recent results and showing 1.7km strike extent**

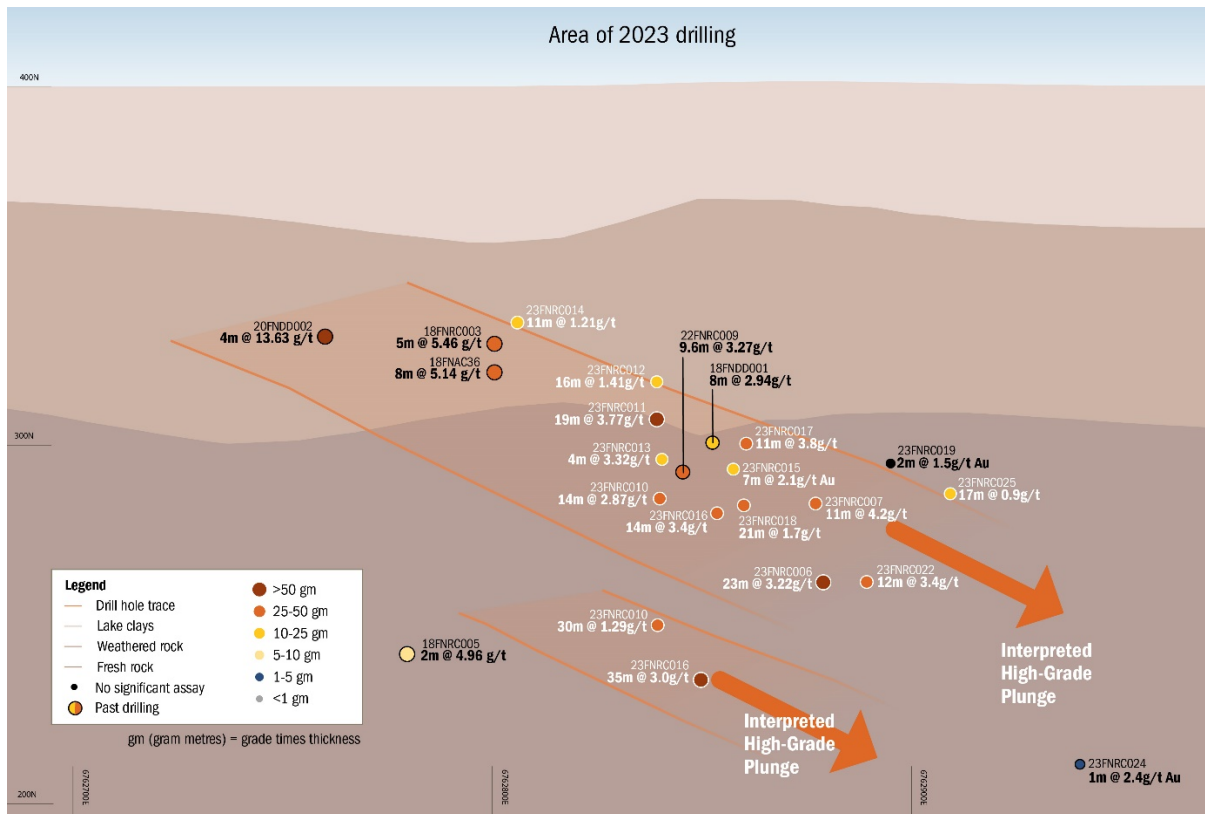


Figure 2: Longitudinal projection of Fortitude North with new drilling showing interpreted high grade plunging shoots

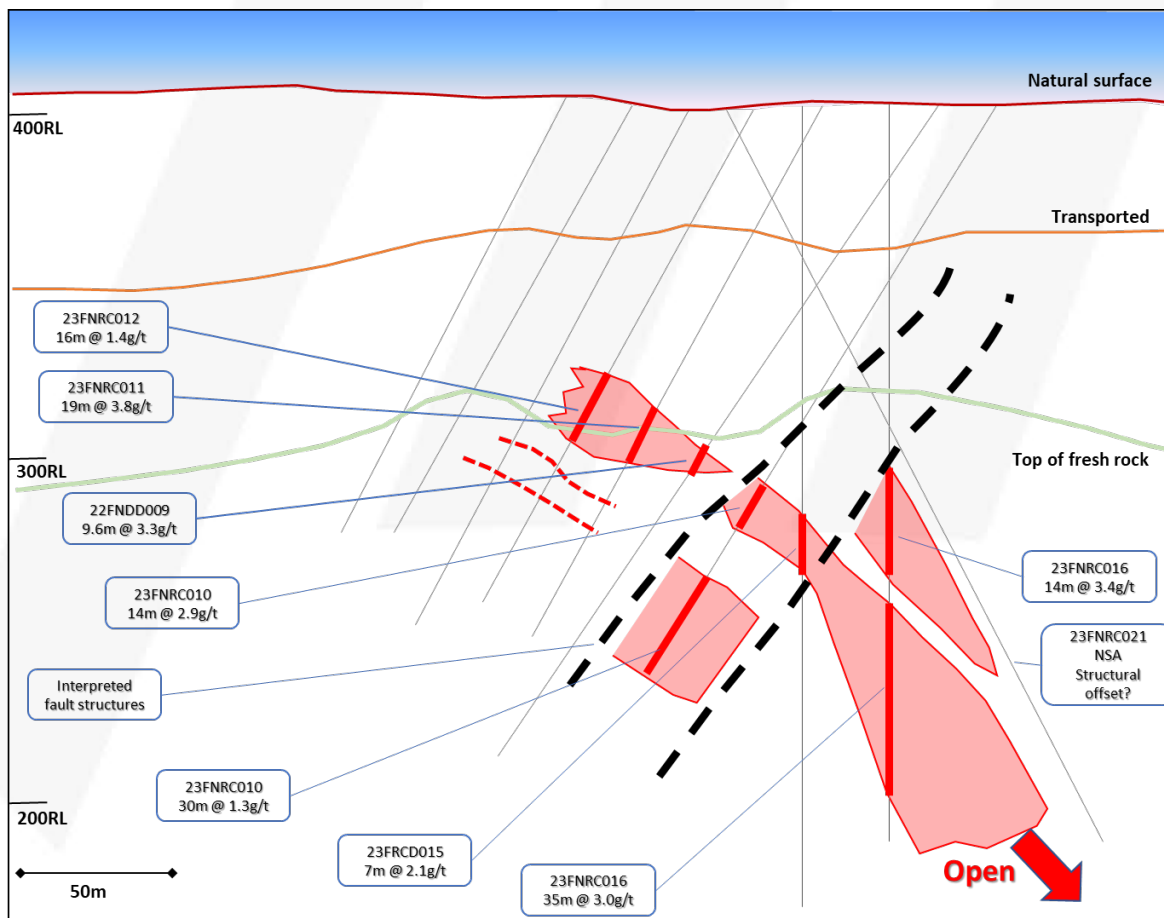


Figure 3: Interpreted drill section at 6762840N showing the best mineralisation is open at depth

## Matsa Executive Chairman Mr Paul Poli commented:

*“These fantastic results speak for themselves and whilst further work is obviously required, we see this as a confirmed significant discovery. In fact, I think Fortitude North will be substantially better than our Fortitude Gold Mine, only 6km to the south, where we have a gold resource of 489,000oz.*

*Matsa’s geology team tell me that they can see multiple phases and styles of mineralisation that speaks to a very long lived system, with up to four gold forming events. Before this drilling, we were targeting another Fortitude, but all this now points to something much more substantial and our target is now much bigger commensurate with these bigger intercepts.*

*With this new information and the fact that mineralisation is still open in the major directions, we are targeting a mineralised system which is potentially in excess of 1Moz\* at Fortitude North, all the ingredients are there.”*

\*There has been insufficient exploration to model a JORC 2012 compliant Mineral Resource Estimate at Fortitude North and it is uncertain that further exploration will successfully result in a Mineral Resource Estimate of any size or that a future mining operation can be achieved.

## DRILLING AND DISCUSSION

This focussed RC drilling program was aimed at providing sufficient drilling coverage to establish a maiden resource for the northern portion of the prospect. Through new logging and geological interpretation, it became evident that the Fortitude North mineralised zone could be extended through additional drilling and the program was amended to test lateral continuity both north and east. In this regard, the drilling has been successful in that lateral extensions that are now proven and importantly, the Fortitude North mineralisation remains open in all directions.

The nature of the drilling and assay results, have highlighted the system’s potential size and scale. The new results all come from the northern end of the 1,700m long zone of basement gold mineralisation initially defined by aircore drilling. More than 700m of the basement gold footprint at the southern end of the mineralised zone, remains untested below aircore refusal.

The full program (holes 23FNRC006 to 23FNRC025) has substantially enhanced the outlook and expectations for Fortitude North following encouraging results outlined in Table 2 below:

| holeid    | pre-January model  | Drilling results | Change (m) | Comment / Assays (Au @ 1g/t cutoff)                     |
|-----------|--------------------|------------------|------------|---|
|           | Expected Intercept | Actual Intercept |            |   |
| 23FNRC006 | 8                  | 25               | 17         | 25m @ 3.3g/t Au from 147m                               |
| 23FNRC007 | 8                  | 17               | 9          | 11m @ 4.2g/t Au from 130m and 6m @ 2.1g/t Au from 148m  |
| 23FNRC008 | 6                  | 1                | -5         | 1m @ 1.1g/t Au from 99m                                 |
| 23FNRC009 | 7                  | 2                | -5         | 2m @ 1.5g/t Au from 115m                                |
| 23FNRC010 | 11                 | 44               | 33         | 14m @ 2.9g/t Au from 130m and 30m @ 1.3g/t Au from 160m |
| 23FNRC011 | 10                 | 22               | 12         | 19m @ 3.8g/t Au from 100m and 3m @ 2.1g/t Au from 134m  |
| 23FNRC012 | 18                 | 20               | 2          | 16m @ 1.4g/t Au from 88m and 4m @ 1.8g/t Au from 124m   |
| 23FNRC013 | 8                  | 4                | -4         | 4m @ 3.3g/t Au from 110m                                |
| 23FNRC014 | 10                 | 13               | 3          | 11m @ 1.2g/t Au from 67m and 2m @ 1.6g/t Au from 105m   |
| 23FNRC015 | 0                  | 7                | 7          | 7m @ 2.1g/t Au from 119m                                |
| 23FNRC016 | 0                  | 49               | 49         | 14m @ 3.4g/t Au from 113m and 35m @ 3.0g/t Au from 150m |
| 23FNRC017 | 13                 | 11               | -2         | 11m @ 3.8g/t Au from 108m                               |
| 23FNRC018 | 0                  | 21               | 21         | 21m @ 1.7g/t Au from 120m                               |
| 23FNRC019 | 6                  | 2                | -4         | 2m @ 1.5g/t Au from 135m                                |
| 23FNRC020 | 0                  | 0                | 0          | NSA (< 1g/t)  |
| 23FNRC021 | 0                  | 0                | 0          | NSA (< 1g/t)  |
| 23FNRC022 | 0                  | 12               | 12         | 12m @ 3.4g/t Au from 143m                               |
| 23FNRC023 | 0                  | 0                | 0          | No lode logged  |
| 23FNRC024 | 0                  | 1                | 1          | 1m @ 2.4g/t Au from 164m                                |
| 23FNRC025 | 0                  | 17               | 17         | 17m @ 0.9g/t Au from 121m                               |

New assay information in blue

**Table 2: Summary of 2023 drilling results outlining upside seen in the drilling program**

Matsa engaged experienced and highly regarded consultant Economic Geologist, Nigel Maund, to inspect these exciting new mineralised intercepts as well as earlier intercepts in diamond drill-core, in order to provide an appraisal of the implications of these drilling results, including mineralisation style and geological characteristics.

The lithologic package which hosts the several stages of gold + quartz + sulphide stockwork vein and vein breccia styles of gold mineralization at Fortitude North, are comprised of variably hydrothermally altered sheared to massive basalts, dolerites and thin grey to black pyritic argillites invaded by late granodioritic to dacitic feldspar porphyry or micro-granitoid dikes. The latter vary from a few tens of centimetres up to two metres in width.

Both the drill core and RC cuttings testify to the nature of the structural architecture of Fortitude North, with this being comprised of multiple discrete to continuous shear zones developed on lithologic boundaries between basaltic lavas, tuffs, dolerite dikes and sills and thin folded units of grey to black argillites. An important fact in this regard, is the interplay between low angle thrust / shears and moderately to steeply dipping structures that likely relate to high grade shoots.

Three key features of the Fortitude North mineralisation were highlighted as follows:

- a) The paucity of lithologies displaying intense shearing compared to those displaying brittle fracture tectonics;
- b) Dominance by stockwork veining and vein breccias;
- c) The unusual dominance of gold mineralised zones by two or even three phases of stockwork veining and / or brecciation of massive fine to medium grained rocks characterised by intense to extreme pervasive albitisation and aphanitic silicification.

Maund, has observed 4 stages of veining and brecciation as evidence of a long lived gold forming system, which strongly supports the potential for Fortitude North to be a major gold deposit.

- An early, Stage 1, mylonitic shear hosted, quartz + pyrite vein system hosted within intensely sheared actinolite + chlorite ± epidote + disseminated magnetite + disseminated pyrite schists in zones varying from ± 20 to 40 m in width; Stage 1 gold mineralised system appears to be developed around more steeply dipping zones of intense (mylonitic) shearing preferentially developed on lithologic contacts between high Mg basalts (chlorite schists) and dolerite. (This geometric disposition of mineralisation bears direct comparison with the various ore bodies described for the Sunrise Dam Gold deposit (SDG) and exhibits the characteristics of the complex shear duplex structures described for the SDG).
- A complex 2nd stage of brittle – ductile, shear controlled gold mineralised tectono – hydrothermal breccia is developed within massive, pervasive, albite + quartz + pyrite + chlorite alteration. Stage 2 gold mineralised appears to be developed along gently dipping (20° - 25°) structures.
- A third mineralising event is characterised by the development of pervasive zones of silicification by mid grey to more rarely a bluish grey glassy quartz + disseminated arsenopyrite + ankerite + sericite (roscoelite) alteration over zones varying from 0.5 to 2 m with gold grades ranging from 5 to 10 g/t Au. This event overprints all earlier gold mineralisation events and is mineralogically like the gold mineralization reported for the SDG.
- A late 4th stage is dominated by milky quartz as irregular veinlets and vein breccias. The mineralisation styles are similar in style to those described for the SDG by Baker et al, 2010 and McLelland et al, 2013.

*Appendix 3 outlines key observations of the mineralisation from both Sunrise Dam and Fortitude North*

Recognition of at least 3 stages of gold-mineralised hydrothermal veins and breccias at Fortitude North emphasises similarities with the giant Sunrise Dam deposit, only 23 km to the north, as described by Baker et al, 2010<sup>1</sup>, McLellan et al, 2013<sup>2</sup> and Porter<sup>3</sup> in their geologic papers and internet articles.

The importance of a complex fault step-over containing both the 12Moz Sunrise Dam and the 8Moz Wallaby deposit was highlighted by Zhang et al 2013 as a major control on these two giant gold deposits (Figure 5). The fault step-over described by Zhang, forms part of a larger regional scale step-over structure which includes Matsa's Fortitude North, Fortitude and Red October deposits and the Lancefield deposit further to the north within the Laverton Tectonic Zone (Figure 5). This complex fault array is interpreted to have been a major control of gold mineralisation in the district.

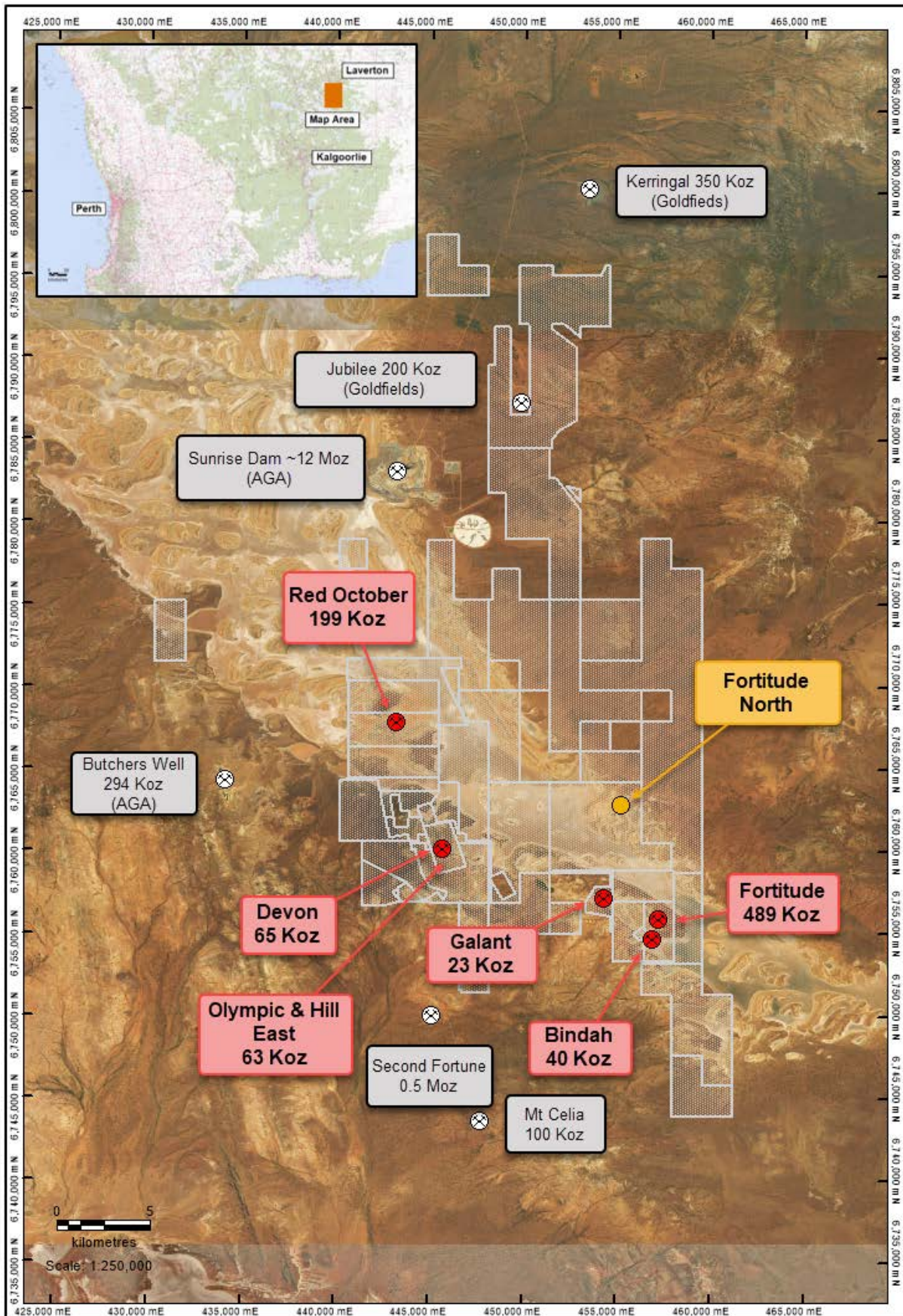


**Photo: Drill site at Fortitude North, April 2023**

<sup>1</sup> Baker T, Bartelli M, Blenkinsop T, Cleverley J S, McLellan J, Nugus M and Gillan D; "P – T – X Conditions of Fluids in the Sunrise Dam Gold Deposit, Western Australia, and Implications for the Interplay between Deformation and Fluids," ECON GEOL 2010, Vol 105, No 5, pp 873 – 886.

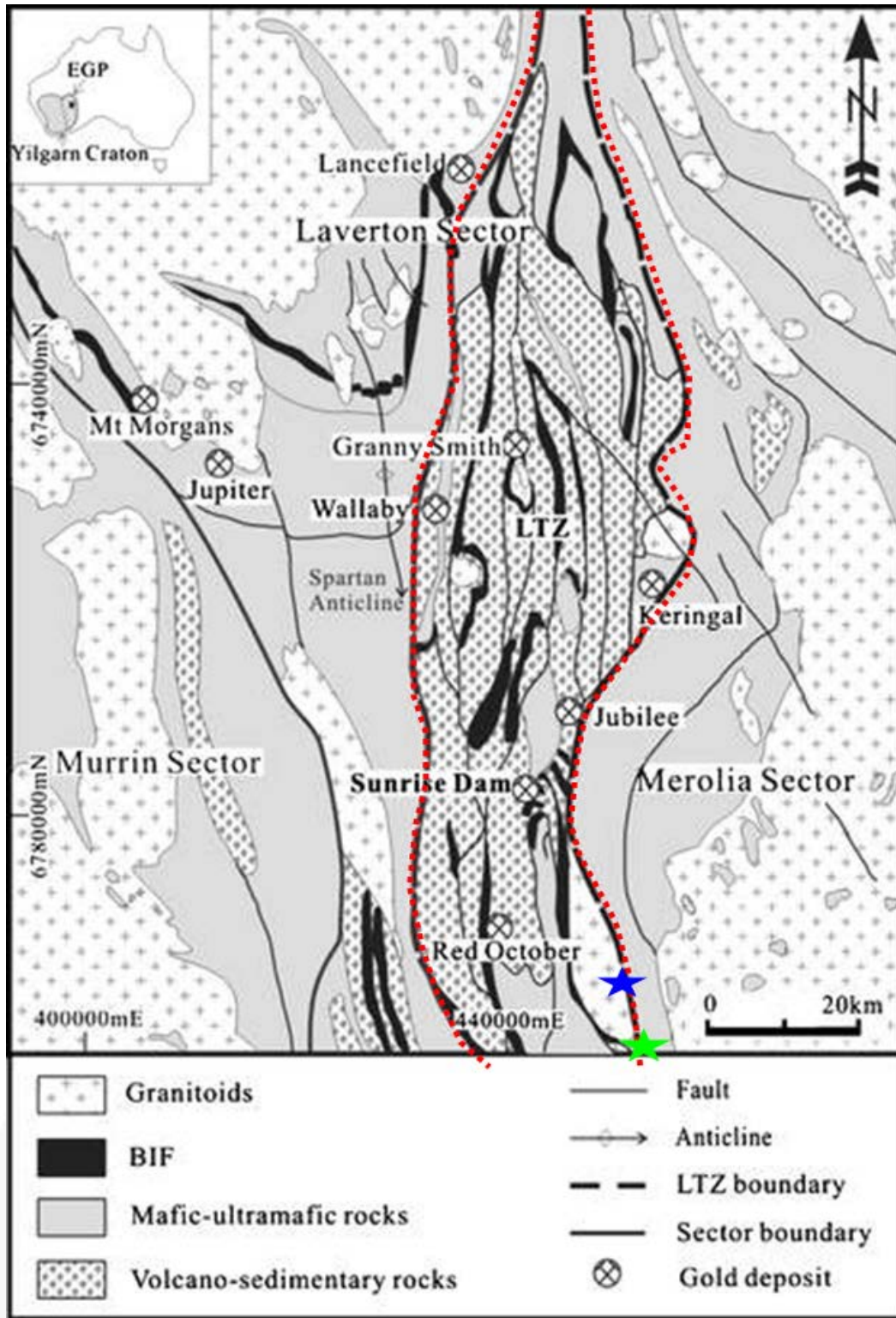
<sup>1</sup> McLellan J G, Blenkinsop T G & Nugus M J; "Fluid Pressure, Geomechanical Evolution and Predictive Targeting of the Sunrise Dam Gold Deposit, Western Australia." World Gold Conference, Brisbane, Queensland, 26 – 29 September 2013

<sup>1</sup> Porter M J; "Sunrise Dam, Sunrise and Cleo Gold Deposits, Western Australia.," PORTERGEO Summary Deposit Report, Internet online



**Figure 4: Matsa’s Lake Carey Gold Project showing the location of the Fortitude North prospect, Fortitude Gold Mine and nearby significant resources.**





**Figure 5:** Simplified geological map of the Laverton Greenstone Belt (modified after Salier<sup>4</sup> et al. 2005), showing the sectors suggested by Cassidy et al. (2002) and the position of Laverton Tectonic Zone (LTZ) that hosts most gold deposits in this area, including Sunrise Dam, Wallaby, Granny Smith, Fortitude North (blue) and Fortitude Gold Mine (green). Inset: the position of the area shown in the map (rectangle) in the Yilgarn Craton and Eastern Goldfield Province (EGP)

<sup>4</sup> Salier, B.P., Groves, D.I., McNaughton, N.J., Fletcher, I.R., 2005. Geochronological and stable isotope evidence for widespread orogenic gold mineralization from a deep-seated fluid source at ca 2.65 Ga in the Laverton Gold Province, Western Australia. *Economic Geology* 100, 1363-1388



*Photo: Drill site at Fortitude North, April 2023*

## **GEOLOGICAL COMPARISONS TO SUNRISE DAM**

Detailed observations of mineralisation in diamond drill core and RC chips by Nigel Maund has been focused on gangue and ore mineralogy of mineralised vein types, timing relationships between veins and vein breccias and distinctive hydrothermal alteration associated with each of them.

The study concluded that Fortitude North is made up of two broadly different episodes of mineralised veins and vein breccias within which, there is evidence of further overprinting relationships between individual veins sets resulting in a multi episodic gold forming geological environment.

- The earliest stage comprises “ribbon” pyritic quartz veins (Type 1 veins) is characterised by ductile textures such as folds (ptygmatic folds) and pinch and swell shapes (boudinage) which are restricted to zones of intense shearing. Gold grades tend to vary from 0.8 to +4 g/t Au depending on the density of veining. Higher gold grades are typically accompanied by the presence of arsenopyrite and carbonate development as shown in Figure 6
- Later mineralisation (Type 2 Veins) characterized by predominantly brittle deformation with development of pyritic quartz crackle veins and breccias with clear overprinting relationships between them into strongly silicified and bleached (albite altered) mafic volcanics (Figure 7)

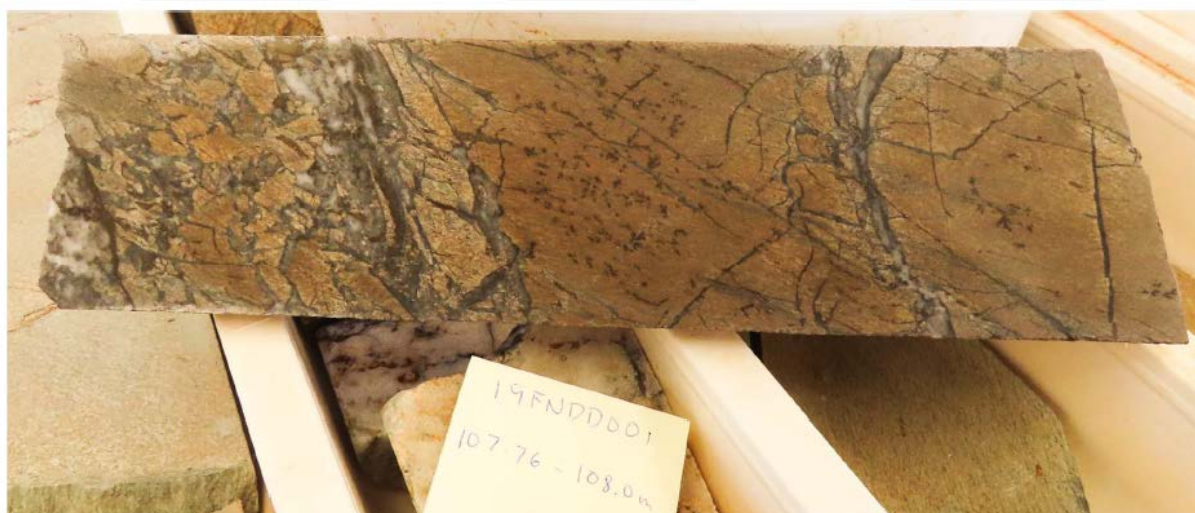
These findings are taken as evidence that gold mineralisation at Fortitude North is the product of multiple stages of deformation and intense hydrothermal activity which were active over a long period of time.

Such strong evidence of the long lived multi-staged nature of mineralisation at Fortitude North has led to speculation about whether these are linked both in space and time, to the processes which led to the formation of the nearby giant gold deposits at Sunrise Dam (SGD) and Wallaby (W) located 25km and 50km respectively, to the north of Fortitude North in the Laverton Tectonic Zone (LTZ). The report

by Maund, presents a comparison between key geological elements at Fortitude North and SGD and concludes that despite differences in host rocks, structural orientation and vein and alteration chemistry, there is a common thread of episodic pulses of gold mineralised veins and vein breccias which makes the likelihood that they are linked to the same deformation events, worthy of closer consideration.



**Figure 6:** Core from 188.22-188.44m depth in diamond drillhole 20FNDD005 illustrates Type 1 ribbon quartz veins in strongly sheared mafic volcanics



**Figure 7:** Core from 107.76 to 108m depth in diamond drillhole 20FNDD001 illustrates Type 2 brittle fracture style of gold mineralisation as crackle veins and vein fill breccia

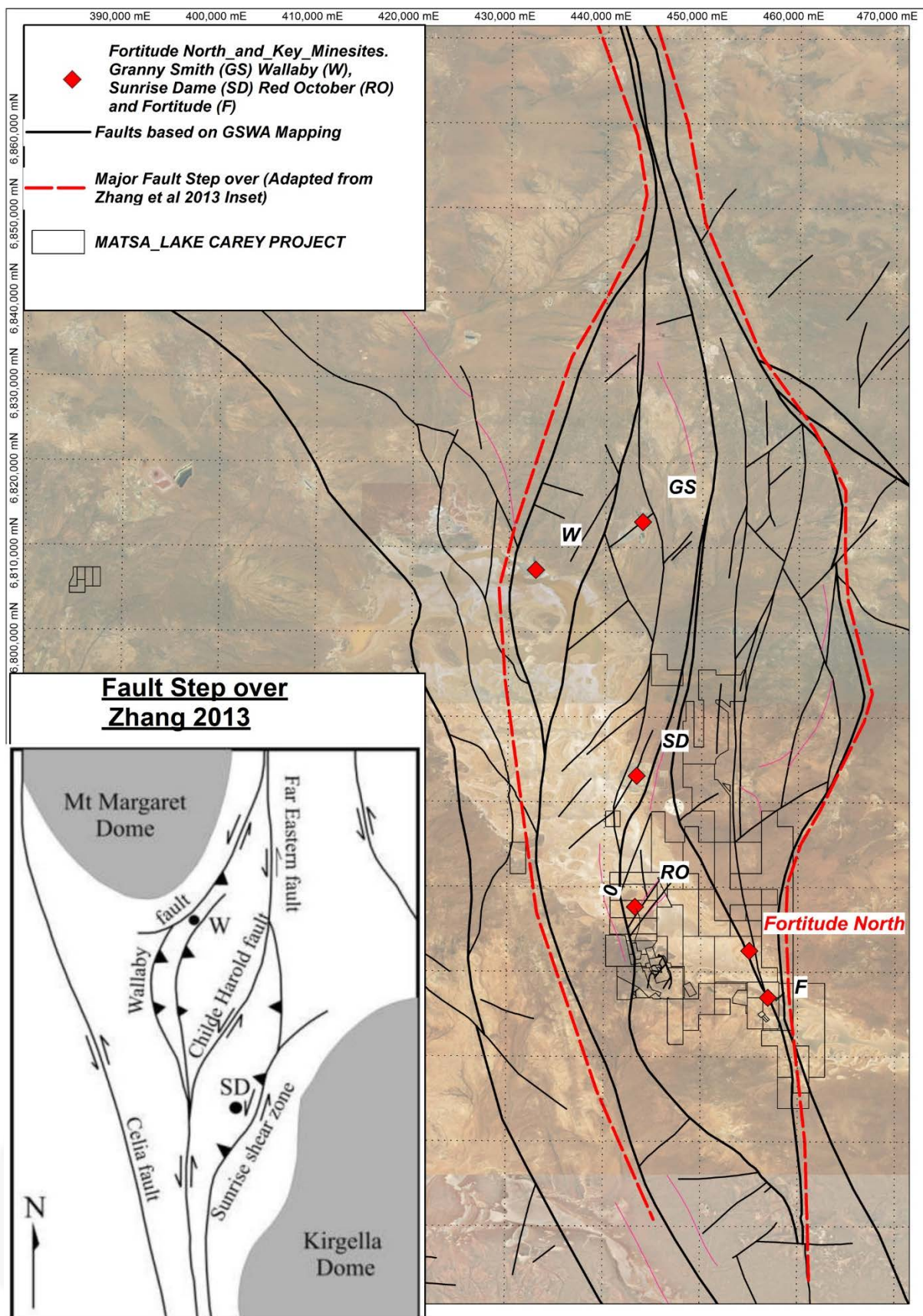
Analysis by Zhang et al (2013) showed that SGD and W are located within a complex fault step over or thrust duplex structure (Figure 8). This study demonstrated that the world class SGD and W gold

deposits are the product of multiple deformation and fault re-activation events within this regional structure. The orientation and nature of individual bodies of mineralisation within these deposits (there are at least 20 orebodies at Sunrise Dam) varied according to the ambient stress regime, and resulting complex interplay between multiple faults, and local fluid sources.

## NEXT STEPS

Key work plan to advance the Fortitude North prospect include:

- Update geological model
- Continue research into application of 3D seismic survey under R&D to improve drill targeting under 40m of cover
- Design next round of drilling
  - it is likely diamond drilling will be required to obtain critical orientation data, associated with the various phases of mineralisation as well as understanding structural complexities seen in the eastern margins of the mineralised system (eg section 6762840N of Figure 2
  - drilling initially focussed on the northern section which can use land based drilling rigs
  - once the northern setting is better understood, progressively work south under the lake where Matsa has identified high grade gold intercepts in previous drilling



**Figure 8** (a) Structural elements of major fault step-over structure related to the giant Sunrise Dam (SD) and Wallaby (W) deposits. (b) Location of SD and W together with Matsa’s Fortitude North (FN), Fortitude (F) and Red October (RO) gold deposits on published GSWA structural data demonstrating their position within this major dilational jog.

## MINERAL RESOURCES

The global Mineral Resource Estimate for the Lake Carey Gold Project remains at **886,000oz @ 2.4g/t Au** as outlined in Table 2 below.

|                             | Cutoff<br>g/t Au | Measured   |            | Indicated    |            | Inferred     |            | Total Resource |            |            |
|-----------------------------|------------------|------------|------------|--------------|------------|--------------|------------|----------------|------------|------------|
|                             |                  | ('000t)    | g/t Au     | ('000t)      | g/t Au     | ('000t)      | g/t Au     | ('000t)        | g/t Au     | ('000 oz)  |
| <b>Red October</b>          |                  |            |            |              |            |              |            |                |            |            |
| Red October UG              | 2.0              | 105        | 8          | 483          | 5.7        | 411          | 6.3        | 999            | 6.2        | 199        |
| <b>Red October Subtotal</b> |                  | <b>105</b> | <b>8.4</b> | <b>483</b>   | <b>5.7</b> | <b>411</b>   | <b>6.3</b> | <b>999</b>     | <b>6.2</b> | <b>199</b> |
| <b>Devon</b>                |                  |            |            |              |            |              |            |                |            |            |
| Devon Pit (OP)              | 1.0              | -          | -          | 341          | 4.8        | 102          | 3.6        | 443            | 4.6        | 65         |
| Olympic (OP)                | 1.0              | -          | -          | -            | -          | 171          | 2.8        | 171            | 2.8        | 15         |
| Hill East (OP)              | 1.0              | -          | -          | -            | -          | 748          | 2.0        | 748            | 2.0        | 48         |
| <b>Devon Subtotal</b>       |                  | <b>-</b>   | <b>-</b>   | <b>341</b>   | <b>4.8</b> | <b>1021</b>  | <b>2.3</b> | <b>1362</b>    | <b>2.9</b> | <b>128</b> |
| <b>Fortitude</b>            |                  |            |            |              |            |              |            |                |            |            |
| Fortitude                   | 1.0              | 127        | 2.2        | 2,979        | 1.9        | 4,943        | 1.9        | 8,048          | 1.9        | 489        |
| Gallant (OP)                | 1.0              | -          | -          | -            | -          | 341          | 2.1        | 341            | 2.1        | 23         |
| Bindah (OP)                 | 1.0              | -          | -          | 43           | 3.3        | 483          | 2.3        | 526            | 2.4        | 40         |
| <b>Fortitude Subtotal</b>   |                  | <b>127</b> | <b>2.2</b> | <b>3021</b>  | <b>2.0</b> | <b>5,767</b> | <b>1.9</b> | <b>8,915</b>   | <b>1.9</b> | <b>553</b> |
| <b>Stockpiles</b>           |                  | <b>-</b>   | <b>-</b>   | <b>-</b>     | <b>-</b>   | <b>191</b>   | <b>1.0</b> | <b>191</b>     | <b>1.0</b> | <b>6</b>   |
| <b>Total</b>                |                  | <b>232</b> | <b>5.0</b> | <b>3,845</b> | <b>2.7</b> | <b>7,199</b> | <b>2.2</b> | <b>11,467</b>  | <b>2.4</b> | <b>886</b> |

**Table 2: Lake Carey Resource\***

\*Matsa confirms that it is not aware of any new information or data that materially affects the Resource as stated. All material assumptions and technical parameters underpinning the Mineral Resource estimate continue to apply and have not changed since the last release.

\***Special note:** The Resources of the Devon Pit project, representing 65koz, are subject to the profit share Joint Venture Agreement announced on 23 December 2022<sup>5</sup>.

This ASX announcement is authorised for release by the Board of Matsa Resources Limited.

For further information please contact:

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### Competent Person Statement

#### Exploration results

The information in this report that relates to Exploration results is based on information and compiled by Pascal Blampain, who is a Member of the Australasian Institute of Mining and Metallurgy and the Australian Institute of Geoscientists. Mr Blampain serves on the Board and is a full time employee, of Matsa Resources Limited. Mr Blampain has sufficient experience which is relevant to the style of mineralisation and the type of ore deposit under consideration and the activities undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Blampain consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

<sup>5</sup> ASX Announcement 23rd December 2022-Settlement of Devon Pit JVA With Linden - Devon Gold Project

## Appendix 1

**Table 2: Collar Details**

| Hole_ID   | Hole_Type | Depth | East   | North   | RL  | Dip | Azimuth | NAT_Grid_ID | Lease_ID |
|-----------|-----------|-------|--------|---------|-----|-----|---------|-------------|----------|
| 23FNRC006 | RC        | 178   | 455180 | 6762880 | 403 | -60 | 270     | MGA94_51    | E39/1864 |
| 23FNRC007 | RC        | 220   | 455220 | 6762880 | 402 | -60 | 269     | MGA94_51    | E39/1864 |
| 23FNRC008 | RC        | 142   | 455121 | 6762841 | 403 | -61 | 269     | MGA94_51    | E39/1864 |
| 23FNRC009 | RC        | 140   | 455138 | 6762841 | 403 | -61 | 270     | MGA94_51    | E39/1864 |
| 23FNRC010 | RC        | 190   | 455250 | 6762840 | 402 | -60 | 267     | MGA94_51    | E39/1864 |
| 23FNRC011 | RC        | 178   | 455200 | 6762840 | 402 | -60 | 269     | MGA94_51    | E39/1864 |
| 23FNRC012 | RC        | 160   | 455180 | 6762840 | 403 | -61 | 269     | MGA94_51    | E39/1864 |
| 23FNRC013 | RC        | 170   | 455161 | 6762840 | 403 | -60 | 268     | MGA94_51    | E39/1864 |
| 23FNRC014 | RC        | 140   | 455121 | 6762800 | 402 | -60 | 270     | MGA94_51    | E39/1864 |
| 23FNRC015 | RC        | 221   | 455195 | 6762840 | 402 | -90 | 269     | MGA94_51    | E39/1864 |
| 23FNRC016 | RC        | 239   | 455221 | 6762842 | 402 | -90 | 0       | MGA94_51    | E39/1864 |
| 23FNRC017 | RC        | 187   | 455199 | 6762863 | 402 | -61 | 269     | MGA94_51    | E39/1864 |
| 23FNRC018 | RC        | 215   | 455185 | 6762864 | 402 | -89 | 129     | MGA94_51    | E39/1864 |
| 23FNRC019 | RC        | 191   | 455200 | 6762880 | 403 | -61 | 269     | MGA94_51    | E39/1864 |
| 23FNRC020 | RC        | 190   | 455193 | 6762882 | 402 | -90 | 148     | MGA94_51    | E39/1864 |
| 23FNRC021 | RC        | 240   | 455170 | 6762840 | 403 | -60 | 90      | MGA94_51    | E39/1864 |
| 23FNRC022 | RC        | 185   | 455194 | 6762899 | 403 | -89 | 130     | MGA94_51    | E39/1864 |
| 23FNRC023 | RC        | 221   | 455232 | 6762921 | 403 | -90 | 70      | MGA94_51    | E39/1864 |
| 23FNRC024 | RC        | 175   | 455182 | 6762923 | 403 | -89 | 242     | MGA94_51    | E39/1864 |
| 23FNRC025 | RC        | 165   | 455166 | 6762924 | 404 | -80 | 275     | MGA94_51    | E39/1864 |

**Table 3: Assay Results >1.00g/t Au**

| Hole_ID   | Depth From | Depth To | Au_Batch_No | Au_ppm |
|-----------|------------|----------|-------------|--------|
| 23FNRC006 | 147        | 148      | KA23007265  | 1.65   |
| 23FNRC006 | 148        | 149      | KA23007265  | 3.76   |
| 23FNRC006 | 149        | 150      | KA23007265  | 6.33   |
| 23FNRC006 | 150        | 151      | KA23007265  | 6.44   |
| 23FNRC006 | 151        | 152      | KA23007265  | 4.91   |
| 23FNRC006 | 152        | 153      | KA23007265  | 2.46   |
| 23FNRC006 | 153        | 154      | KA23007265  | 1.16   |
| 23FNRC006 | 158        | 159      | KA23007265  | 5.71   |
| 23FNRC006 | 159        | 160      | KA23007265  | 7.12   |
| 23FNRC006 | 160        | 161      | KA23007265  | 10.60  |
| 23FNRC006 | 161        | 162      | KA23007265  | 3.66   |
| 23FNRC006 | 162        | 163      | KA23007265  | 1.06   |
| 23FNRC006 | 165        | 166      | KA23007265  | 3.14   |
| 23FNRC006 | 167        | 168      | KA23007265  | 7.61   |
| 23FNRC006 | 169        | 170      | KA23007265  | 5.15   |
| 23FNRC006 | 170        | 171      | KA23007265  | 1.58   |
| 23FNRC006 | 171        | 172      | KA23007265  | 1.39   |
| 23FNRC007 | 130        | 131      | KA23007265  | 1.44   |
| 23FNRC007 | 131        | 132      | KA23007265  | 2.04   |
| 23FNRC007 | 132        | 133      | KA23007265  | 2.68   |
| 23FNRC007 | 133        | 134      | KA23007265  | 3.85   |
| 23FNRC007 | 134        | 135      | KA23007265  | 6.42   |
| 23FNRC007 | 135        | 136      | KA23007265  | 5.38   |
| 23FNRC007 | 136        | 137      | KA23007265  | 6.99   |
| 23FNRC007 | 137        | 138      | KA23007265  | 8.11   |
| 23FNRC007 | 138        | 139      | KA23007265  | 5.52   |
| 23FNRC007 | 139        | 140      | KA23007265  | 2.23   |
| 23FNRC007 | 140        | 141      | KA23007265  | 1.57   |
| 23FNRC007 | 148        | 149      | KA23007265  | 1.72   |
| 23FNRC007 | 149        | 150      | KA23007265  | 3.71   |
| 23FNRC007 | 150        | 151      | KA23007265  | 2.77   |
| 23FNRC007 | 151        | 152      | KA23007265  | 1.69   |
| 23FNRC007 | 152        | 153      | KA23007265  | 1.56   |
| 23FNRC007 | 153        | 154      | KA23007265  | 1.16   |
| 23FNRC008 | 99         | 100      | KA23035727  | 1.09   |
| 23FNRC009 | 115        | 116      | KA23011178  | 1.74   |
| 23FNRC009 | 116        | 117      | KA23011178  | 1.32   |
| 23FNRC010 | 86         | 87       | KA23059245  | 1.78   |
| 23FNRC010 | 87         | 88       | KA23059245  | 1.91   |
| 23FNRC010 | 130        | 131      | KA23011513  | 5.48   |
| 23FNRC010 | 131        | 132      | KA23035727  | 3.96   |
| 23FNRC010 | 132        | 133      | KA23011513  | 3.13   |
| 23FNRC010 | 133        | 134      | KA23011513  | 3.09   |
| 23FNRC010 | 134        | 135      | KA23011513  | 3.25   |
| 23FNRC010 | 135        | 136      | KA23011513  | 2.34   |
| 23FNRC010 | 136        | 137      | KA23011513  | 1.49   |
| 23FNRC010 | 137        | 138      | KA23011513  | 1.26   |
| 23FNRC010 | 138        | 139      | KA23011513  | 3.21   |



|           |     |     |            |      |
|-----------|-----|-----|------------|------|
| 23FNRC010 | 140 | 141 | KA23011513 | 4.67 |
| 23FNRC010 | 141 | 142 | KA23011513 | 1.01 |
| 23FNRC010 | 143 | 144 | KA23011513 | 3.45 |
| 23FNRC010 | 148 | 149 | KA23011513 | 1.01 |
| 23FNRC010 | 151 | 152 | KA23011513 | 1.92 |
| 23FNRC010 | 154 | 155 | KA23011513 | 1.88 |
| 23FNRC010 | 160 | 161 | KA23011513 | 4.38 |
| 23FNRC010 | 164 | 165 | KA23011513 | 1.18 |
| 23FNRC010 | 165 | 166 | KA23011513 | 1.57 |
| 23FNRC010 | 167 | 168 | KA23011513 | 1.17 |
| 23FNRC010 | 176 | 177 | KA23011513 | 1.11 |
| 23FNRC010 | 177 | 178 | KA23011513 | 1.41 |
| 23FNRC010 | 178 | 179 | KA23011513 | 3.09 |
| 23FNRC010 | 179 | 180 | KA23011513 | 1.22 |
| 23FNRC010 | 180 | 181 | KA23011513 | 1.57 |
| 23FNRC010 | 182 | 183 | KA23011513 | 1.58 |
| 23FNRC010 | 183 | 184 | KA23011513 | 1.08 |
| 23FNRC010 | 184 | 185 | KA23011513 | 2.54 |
| 23FNRC010 | 188 | 189 | KA23011513 | 1.16 |
| 23FNRC010 | 189 | 190 | KA23011513 | 1.07 |
| 23FNRC011 | 100 | 101 | KA23011513 | 4.47 |
| 23FNRC011 | 101 | 102 | KA23011513 | 6.54 |
| 23FNRC011 | 102 | 103 | KA23011513 | 4.92 |
| 23FNRC011 | 103 | 104 | KA23011513 | 4.53 |
| 23FNRC011 | 104 | 105 | KA23011513 | 4.42 |
| 23FNRC011 | 105 | 106 | KA23011513 | 4.72 |
| 23FNRC011 | 109 | 110 | KA23011513 | 1.56 |
| 23FNRC011 | 110 | 111 | KA23011513 | 1.72 |
| 23FNRC011 | 111 | 112 | KA23011513 | 8.07 |
| 23FNRC011 | 112 | 113 | KA23011513 | 8.81 |
| 23FNRC011 | 113 | 114 | KA23011513 | 4.46 |
| 23FNRC011 | 114 | 115 | KA23011513 | 1.57 |
| 23FNRC011 | 115 | 116 | KA23011513 | 2.54 |
| 23FNRC011 | 116 | 117 | KA23011513 | 1.21 |
| 23FNRC011 | 117 | 118 | KA23011513 | 1.03 |
| 23FNRC011 | 118 | 119 | KA23011513 | 1.02 |
| 23FNRC011 | 135 | 136 | KA23011513 | 1.59 |
| 23FNRC012 | 88  | 89  | KA23012035 | 1.14 |
| 23FNRC012 | 89  | 90  | KA23012035 | 1.12 |
| 23FNRC012 | 91  | 92  | KA23012035 | 3.93 |
| 23FNRC012 | 94  | 95  | KA23012035 | 1.14 |
| 23FNRC012 | 97  | 98  | KA23012035 | 3.35 |
| 23FNRC012 | 98  | 99  | KA23012035 | 2.42 |
| 23FNRC012 | 101 | 102 | KA23012035 | 2.46 |
| 23FNRC012 | 124 | 125 | KA23012035 | 1.48 |
| 23FNRC012 | 126 | 127 | KA23012035 | 1.77 |
| 23FNRC012 | 127 | 128 | KA23012035 | 1.15 |
| 23FNRC013 | 110 | 111 | KA23013028 | 1.78 |
| 23FNRC013 | 111 | 112 | KA23013028 | 1.66 |
| 23FNRC013 | 112 | 113 | KA23013028 | 6.27 |

|           |     |     |             |      |
|-----------|-----|-----|-------------|------|
| 23FNRC013 | 113 | 114 | KA23013028  | 3.56 |
| 23FNRC014 | 67  | 68  | KA23013003  | 2.13 |
| 23FNRC014 | 69  | 70  | KA23013003  | 3.72 |
| 23FNRC014 | 74  | 75  | KA23013003  | 1.43 |
| 23FNRC014 | 76  | 77  | KA23013003  | 1.23 |
| 23FNRC014 | 77  | 78  | KA23013003  | 1.04 |
| 23FNRC014 | 105 | 106 | KA23013003  | 1.35 |
| 23FNRC014 | 106 | 107 | KA23013003  | 1.85 |
| 23FNRC014 | 116 | 117 | KA23013003  | 1.56 |
| 23FNRC015 | 119 | 120 | KGI23-10282 | 1.86 |
| 23FNRC015 | 120 | 121 | KGI23-10282 | 3.52 |
| 23FNRC015 | 121 | 122 | KGI23-10282 | 3.05 |
| 23FNRC015 | 122 | 123 | KGI23-10282 | 1.31 |
| 23FNRC015 | 123 | 124 | KGI23-10282 | 1.32 |
| 23FNRC015 | 124 | 125 | KGI23-10282 | 1.68 |
| 23FNRC015 | 125 | 126 | KGI23-10282 | 1.72 |
| 23FNRC015 | 133 | 134 | KGI23-10282 | 2.85 |
| 23FNRC015 | 139 | 140 | KGI23-10282 | 1.91 |
| 23FNRC015 | 152 | 153 | KGI23-10282 | 1.12 |
| 23FNRC015 | 153 | 154 | KGI23-10282 | 1.11 |
| 23FNRC015 | 206 | 207 | KGI23-10282 | 1.02 |
| 23FNRC016 | 103 | 104 | KGI23-10282 | 1.05 |
| 23FNRC016 | 106 | 107 | KGI23-10282 | 2.09 |
| 23FNRC016 | 107 | 108 | KGI23-10282 | 3.92 |
| 23FNRC016 | 113 | 114 | KGI23-10282 | 3.78 |
| 23FNRC016 | 114 | 115 | KGI23-10282 | 9.03 |
| 23FNRC016 | 115 | 116 | KGI23-10282 | 6.96 |
| 23FNRC016 | 117 | 118 | KGI23-10282 | 3.62 |
| 23FNRC016 | 118 | 119 | KGI23-10282 | 2.78 |
| 23FNRC016 | 121 | 122 | KGI23-10282 | 3.56 |
| 23FNRC016 | 122 | 123 | KGI23-10282 | 4.45 |
| 23FNRC016 | 123 | 124 | KGI23-10282 | 3.49 |
| 23FNRC016 | 124 | 125 | KGI23-10282 | 1.16 |
| 23FNRC016 | 126 | 127 | KGI23-10282 | 1.51 |
| 23FNRC016 | 150 | 151 | KGI23-10282 | 1.26 |
| 23FNRC016 | 153 | 154 | KGI23-10282 | 9.98 |
| 23FNRC016 | 154 | 155 | KGI23-10282 | 8.38 |
| 23FNRC016 | 155 | 156 | KGI23-10282 | 4.22 |
| 23FNRC016 | 156 | 157 | KGI23-10282 | 3.22 |
| 23FNRC016 | 158 | 159 | KGI23-10282 | 1.86 |
| 23FNRC016 | 159 | 160 | KGI23-10282 | 1.38 |
| 23FNRC016 | 160 | 161 | KGI23-10282 | 1.79 |
| 23FNRC016 | 164 | 165 | KGI23-10282 | 2.84 |
| 23FNRC016 | 165 | 166 | KGI23-10282 | 9.66 |
| 23FNRC016 | 166 | 167 | KGI23-10351 | 3.57 |
| 23FNRC016 | 167 | 168 | KGI23-10351 | 1.86 |
| 23FNRC016 | 168 | 169 | KGI23-10351 | 1.93 |
| 23FNRC016 | 169 | 170 | KGI23-10351 | 1.45 |
| 23FNRC016 | 170 | 171 | KGI23-10351 | 9.73 |
| 23FNRC016 | 171 | 172 | KGI23-10351 | 5.77 |

|           |                       |     |             |       |
|-----------|-----------------------|-----|-------------|-------|
| 23FNRC016 | 172                   | 173 | KGI23-10351 | 2.58  |
| 23FNRC016 | 174                   | 175 | KGI23-10351 | 4.88  |
| 23FNRC016 | 176                   | 177 | KGI23-10351 | 1.97  |
| 23FNRC016 | 178                   | 179 | KGI23-10351 | 1.45  |
| 23FNRC016 | 179                   | 180 | KGI23-10351 | 1.42  |
| 23FNRC016 | 180                   | 181 | KGI23-10351 | 3.06  |
| 23FNRC016 | 181                   | 182 | KGI23-10351 | 2.13  |
| 23FNRC016 | 182                   | 183 | KGI23-10351 | 1.89  |
| 23FNRC016 | 183                   | 184 | KGI23-10351 | 2.37  |
| 23FNRC016 | 184                   | 185 | KGI23-10351 | 1.35  |
| 23FNRC017 | 108                   | 109 | KGI23-10351 | 3.80  |
| 23FNRC017 | 109                   | 110 | KGI23-10351 | 9.14  |
| 23FNRC017 | 110                   | 111 | KGI23-10351 | 3.37  |
| 23FNRC017 | 111                   | 112 | KGI23-10351 | 2.28  |
| 23FNRC017 | 112                   | 113 | KGI23-10351 | 1.92  |
| 23FNRC017 | 113                   | 114 | KGI23-10351 | 4.28  |
| 23FNRC017 | 114                   | 115 | KGI23-10351 | 2.73  |
| 23FNRC017 | 115                   | 116 | KGI23-10351 | 7.82  |
| 23FNRC017 | 116                   | 117 | KGI23-10351 | 3.22  |
| 23FNRC017 | 117                   | 118 | KGI23-10351 | 1.66  |
| 23FNRC017 | 118                   | 119 | KGI23-10351 | 1.49  |
| 23FNRC018 | 120                   | 121 | KGI23-10412 | 2.54  |
| 23FNRC018 | 121                   | 122 | KGI23-10412 | 2.15  |
| 23FNRC018 | 122                   | 123 | KGI23-10412 | 1.53  |
| 23FNRC018 | 123                   | 124 | KGI23-10412 | 2.29  |
| 23FNRC018 | 124                   | 125 | KGI23-10412 | 1.57  |
| 23FNRC018 | 126                   | 127 | KGI23-10412 | 2.27  |
| 23FNRC018 | 127                   | 128 | KGI23-10412 | 1.36  |
| 23FNRC018 | 128                   | 129 | KGI23-10412 | 1.62  |
| 23FNRC018 | 132                   | 133 | KGI23-10412 | 5.01  |
| 23FNRC018 | 133                   | 134 | KGI23-10412 | 1.91  |
| 23FNRC018 | 134                   | 135 | KGI23-10412 | 1.73  |
| 23FNRC018 | 138                   | 139 | KGI23-10412 | 1.37  |
| 23FNRC018 | 139                   | 140 | KGI23-10412 | 5.07  |
| 23FNRC018 | 140                   | 141 | KGI23-10412 | 1.68  |
| 23FNRC018 | 164                   | 165 | KGI23-10412 | 1.41  |
| 23FNRC018 | 173                   | 174 | KGI23-10412 | 1.41  |
| 23FNRC019 | 119                   | 120 | KGI23-10437 | 1.43  |
| 23FNRC019 | 130                   | 131 | KGI23-10437 | 1.07  |
| 23FNRC019 | 135                   | 136 | KGI23-10437 | 1.62  |
| 23FNRC019 | 136                   | 137 | KGI23-10437 | 1.45  |
| 23FNRC020 | No significant assays |     |             |       |
| 23FNRC021 | No significant assays |     |             |       |
| 23FNRC022 | 143                   | 144 | KGI23-10547 | 2.11  |
| 23FNRC022 | 144                   | 145 | KGI23-10547 | 13.89 |
| 23FNRC022 | 145                   | 146 | KGI23-10547 | 1.76  |
| 23FNRC022 | 146                   | 147 | KGI23-10547 | 1.17  |
| 23FNRC022 | 147                   | 148 | KGI23-10547 | 6.02  |
| 23FNRC022 | 148                   | 149 | KGI23-10547 | 6.03  |
| 23FNRC022 | 151                   | 152 | KGI23-10547 | 1.19  |

|           |                       |     |             |      |
|-----------|-----------------------|-----|-------------|------|
| 23FNRC022 | 152                   | 153 | KGI23-10547 | 1.48 |
| 23FNRC022 | 153                   | 154 | KGI23-10547 | 2.57 |
| 23FNRC022 | 154                   | 155 | KGI23-10547 | 3.02 |
| 23FNRC023 | No significant assays |     |             |      |
| 23FNRC024 | 140                   | 141 | KGI23-10549 | 1.41 |
| 23FNRC024 | 153                   | 154 | KGI23-10549 | 1.14 |
| 23FNRC024 | 164                   | 165 | KGI23-10549 | 2.37 |
| 23FNRC025 | 121                   | 122 | KGI23-10549 | 2.79 |
| 23FNRC025 | 124                   | 125 | KGI23-10549 | 1.05 |
| 23FNRC025 | 125                   | 126 | KGI23-10549 | 1.47 |
| 23FNRC025 | 127                   | 128 | KGI23-10549 | 1.38 |
| 23FNRC025 | 137                   | 138 | KGI23-10549 | 1.93 |
| 23FNRC025 | 138                   | 139 | KGI23-10549 | 2.13 |
| 23FNRC025 | 149                   | 150 | KGI23-10549 | 2.07 |

## Appendix 2 - Matsa Resources Limited

### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

| Criteria                     | JORC Code explanation   | Commentary   |
|------------------------------|---|--|
| <b>Sampling techniques</b>   | <ul style="list-style-type: none"> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.</li> </ul>   | <p>RC samples were collected directly off the drill rig cyclone in pre-numbered calico sample bags after passing through a rig mounted cone splitter. The splitter and cyclone were free flowing at all times and were cleaned at the end of each rod.</p> <p>3 metre composite samples were taken while drilling through the transported overburden using a scoop. All composite samples that assay &gt;0.1g/t Au will have the original 1m splits assayed at a later date.</p> |
|                              | <ul style="list-style-type: none"> <li>Measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> </ul>  | <p>Duplicate sample were taken every 20m and the assays compared to the original.</p>  |
|                              | <ul style="list-style-type: none"> <li>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul> | <p>Samples up to 3kg were pulverised to produce a 30g charge for fire assay. Samples &gt;3kg were split prior to pulverization.</p>  |
| <b>Drilling techniques</b>   | <ul style="list-style-type: none"> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).</li> </ul>   | <p>Drilling was carried out using a truck mounted RG rig and face sampling hammer.</p>   |
| <b>Drill sample recovery</b> | <ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> </ul>   | <p>Sample recovery was determined as being appropriate if the bulk residue volume was reasonably consistent.</p>   |
|                              | <ul style="list-style-type: none"> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> </ul>   | <p>Every effort was made to clean sample system at the end of each 6m rod. The cyclone was kept free flowing even when samples became wet. Drill penetration was paused at each meter if the samplers could not keep up.</p>   |

| Criteria  | JORC Code explanation   | Commentary  |
|---|---|---|
|   | <ul style="list-style-type: none"> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>  | Not applicable, no relationship between sample recovery and grade has been identified.  |
| <b>Logging</b>  | <ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>   | <p>All holes were logged for colour, lithology, regolith, alteration, mineralization and texture directly into Logchief software using standard geological logging codes.</p> <p>Logging is qualitative in nature and washed samples were stored in chip trays and photographed.</p> <p>All sample intervals were logged.</p>   |
| <b>Sub-sampling techniques and sample preparation</b> | <ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples</li> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul> | <p>Not applicable.</p> <p>Samples were collected directly off a rig mounted cone splitter in calico sample bags. When samples became wet the cyclone was kept free flowing. Composite samples were collected using a scoop from bagged RC residues. The 1m original samples were stored for later assay if required.</p> <p>All samples dried and subject to conventional crushing and pulverizing appropriate for 30g fire assay.</p> <p>Matsa employed detailed QAQC procedures utilising field duplicates every 20m as well as having standard and blank samples inserted into the sample sequence.</p> <p>Field duplicates were taken every 20m and compared with the original results.</p> <p>Sample weights of 2-3kg are adequate for gold.</p> |
| <b>Quality of assay data and</b>                      | <ul style="list-style-type: none"> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> </ul>  | 30g fire assay is standard for gold and considered total.   |

| Criteria                                     | JORC Code explanation  | Commentary  |
|--|--|---|
| <b>laboratory tests</b>                      | <ul style="list-style-type: none"> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie. lack of bias) and precision have been established.</li> </ul> | <p>Not Applicable.</p> <p>The use of standards, blanks and field duplicates have established that there is no significant bias cause by sampling or laboratory procedures and an appropriate level of precision has been established.</p> |
| <b>Verification of sampling and assaying</b> | <ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> </ul>  | All assay and sampling procedures have been verified by Company personnel. All results reviewed and cross checked internally.   |
|  | <ul style="list-style-type: none"> <li>The use of twinned holes.</li> </ul>  | No twinned holes were completed.  |
|  | <ul style="list-style-type: none"> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> </ul>   | Geological and sampling data recorded using Logchief software in the field. Data was verified both in the database as well as in section and plan.  |
| <b>Location of data points</b>               | <ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> </ul>  | Collar location was set out using a DGPS and after completion of the program will be picked up by DGPS accurate to 10cm   |
|  | <ul style="list-style-type: none"> <li>Specification of the grid system used.</li> </ul>   | GDA94 UTM co-ordinate system Zone 51.   |
|  | <ul style="list-style-type: none"> <li>Quality and adequacy of topographic control.</li> </ul>   | DGPS set out and pickups are accurate to 10cm.  |
| <b>Data spacing and distribution</b>         | <ul style="list-style-type: none"> <li>Data spacing for reporting of Exploration Results.</li> </ul>   | Drill hole spacing for this program varies between 40m x 40m and 20m x 20m.   |
|  | <ul style="list-style-type: none"> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> </ul>   | Not Applicable, no Mineral Resource or Ore Reserve figure have been quoted from this drilling.  |
|  | <ul style="list-style-type: none"> <li>Whether sample compositing has been applied.</li> </ul>   | Samples were composited to 3 metres only in the barren transported overburden.  |

| Criteria   | JORC Code explanation  | Commentary  |
|--|--|---|
| <b>Orientation of data in relation to geological structure</b> | <ul style="list-style-type: none"> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> </ul>   | The lode orientation was determined by previous RC and Diamond drilling. Drilling was planned to intersect both the primary lodes and supergene mineralization at a high angle.   |
|  | <ul style="list-style-type: none"> <li>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul> | Drilling was planned to intersect both the primary lodes and supergene mineralisation at a high angle.  |
| <b>Sample security</b>   | <ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>  | Samples are delivered directly to the laboratory in Kalgoorlie by Matsa Staff. Sample submission (chain of custody) forms were completed and verified with the samples delivered by laboratory staff. Any discrepancies were corrected prior to sample preparation and assay. |
| <b>Audits or reviews</b>                                       | <ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>  | Not applicable, no audit carried out.   |

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

| Criteria                                       | JORC Code explanation  | Commentary   |
|--|--|--|
| <b>Mineral tenement and land tenure status</b> | <ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</li> </ul> | Exploration was carried out over the following tenements: E39/1864, the tenement is 100% held by Matsa Gold Ltd, a wholly owned subsidiary of Matsa Resources Ltd. |
| <b>Exploration done by other parties</b>       | <ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>  | Not applicable.  |
| <b>Geology</b>                                 | <ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>  | Drilling was carried out based on a target concept of orogenic gold mineralisation along major NNW trending shear zones including the Fortitude Fault.             |



| Criteria  | JORC Code explanation   | Commentary   |
|---|---|--|
| <b>Drill hole Information</b>   | <ul style="list-style-type: none"> <li>• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all material drill holes:               <ul style="list-style-type: none"> <li>○ easting and northing of the drill hole collar</li> <li>○ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>○ dip and azimuth of the hole</li> <li>○ down hole length and interception depth</li> <li>○ hole length.</li> </ul> </li> <li>• If the exclusion of this information is justified on the basis that the information is not material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul> | <p>Drill hole information including set out co-ordinates, dip, azimuth and hole depths are tabled in Appendix 1 of this report.</p> <p>Not applicable, no significant information was excluded.</p>  |
| <b>Data aggregation methods</b>   | <ul style="list-style-type: none"> <li>• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg. cutting of high grades) and cut-off grades are usually material and should be stated.</li> <li>• Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>• The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>  | <p>Gold results were averaged to a cut-off of 0.5g/t and included up to 2m of internal waste. No high grade cuts were applied.</p> <p>Short lengths of high grade results &gt;3g/t Au were reported within larger lower grade intersections. Where this occurred, it was clearly noted in the report as “including”.</p> <p>Not Applicable, no metal equivalents have been used.</p> |
| <b>Relationship between mineralisation widths and intercept lengths</b> | <ul style="list-style-type: none"> <li>• These relationships are particularly important in the reporting of Exploration Results.</li> <li>• If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>• If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg ‘down hole length, true width not known’).</li> </ul>   | <p>All intercepts quoted relate to downhole depth and true widths have not been quoted.</p> <p>Drilling was planned to intersect the mineralisation at a high angle, however true widths still have not been reported.</p> <p>Intercepts are expressed in downhole metres.</p>   |
| <b>Diagrams</b>   | <ul style="list-style-type: none"> <li>• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>   | <p>Appropriate maps and sections have been included in the body of the report.</p>   |

| Criteria                                  | JORC Code explanation   | Commentary  |
|---|---|---|
| <b>Balanced reporting</b>                 | <ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>   | All drill intercepts >1 g/t Au are reported and tabled in Appendix 1.   |
| <b>Other substantive exploration data</b> | <ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul> | Not applicable, no other substantive data is being reported.  |
| <b>Further work</b>                       | <ul style="list-style-type: none"> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>                                       | The nature of further work is discussed in the report including the completion of the current drilling program as a priority. |

Appendix 2

A Comparative Geologic Study between the key characteristics of Sunrise Dam Gold Deposit and the Fortitude North Gold project

| Geologic Features   | Sunrise Dam   | Fortitude North   |
|---|---|---|
| <b>Geologic Structural Regime</b>   | Complex Multistage Shear Duplex   | Complex Multistage Shear Duplex   |
| <b>Key Structural Controls</b>  | Controlled within a NE structural corridor measuring 4.5 to 5 km in strike extent   | Controlled within a structural corridor extending over 1.6 km. However, it is open along strike in both directions  |
|   | The twenty defined gold orebodies are centred upon a series of parallel, gently dipping (~ 30°), and NE – trending shear zones with a thrust duplex architecture and high-strain character.   | Suggestion of both gently NE dipping mineralized NNW (?) striking structures and steeply dipping mineralised structures suggesting the presence of a low angle thrust duplex.   |
| <b>Number of Deformation Events</b>   | Four recognised deformation events D1 to D4 (divided into (a) and (b)). The earliest deformation (D <sub>1</sub> ) formed F <sub>1</sub> folds and thrusts in response to N – S directed compression and shortening (S <sub>1</sub> ). The second event (D <sub>2</sub> ) was characterised by regional E – W shortening associated with the formation of the regional Spartan Anticline. The two following stages, D <sub>3</sub> and D <sub>4</sub> , were responsible for the bulk of the gold mineralisation. D <sub>3</sub> produced major shearing and / or fault because of deformation caused by NNW – SSE to NW – SE orientated stress. This event was responsible for the reactivation of S <sub>1</sub> and S <sub>2</sub> with sinistral strike slip movement as well as development of mineralised S <sub>3</sub> fractures and NE striking extensional vein arrays. | At least three and, most likely, four deformation events although the structural architecture is not understood. Age relationships between the various deformation stages remains to be established and fully documented. Likely there are two main deformation events with D <sub>2</sub> mineralisation separated by a hiatus between the later D <sub>3</sub> and D <sub>4</sub> events. The styles of mineralisation between D <sub>2</sub> and D <sub>3</sub> & D <sub>4</sub> are substantial in terms mineralisation style and hydrothermal alteration mineralogy. |
| <b>Influence of several deformation events on gold mineralization with multi- stage gold mineralization</b> | The D1 and D2 deformation stages were associated with hydrothermal alteration of the rocks by carbonate + chlorite + sericite attended by low grade gold mineralization of typically < 1 g/t Au.<br><br>The D3 and D4 veins differ in terms of mineralogy, texture, and their geochemical signatures. The vein  | Interpreted D2 mineralization is characterised by the formation of a 0.5 to 5 vol% system of sheeted quartz + chlorite veins / veinlets hosted within intensely sheared quartz + Fe chlorite + epidote + disseminated pyritic schists. The gold grade in this style of mineralisation varies from 0.5 to  |

|                                 |   |  |
|---------------------------------|---|--|
|                                 | <p>filling consists of quartz and carbonates in various proportions. Quartz predominates in the D<sub>4b</sub> veins. Pyrite is the main ore mineral present in all veins with arsenopyrite being particularly rich in D<sub>4a</sub>, and base metal sulphides and Pb – Sb sulfosalts found in D<sub>4b</sub> veins. Tellurides are present in both types of D<sub>4</sub> veins, but it is particularly abundant in the D<sub>4b</sub> veins. Coarse native gold is common in the D<sub>4a</sub> veins. Evidence of overlap between D<sub>4</sub> and D<sub>3</sub> events / stages are ubiquitous. D<sub>4</sub> veinlets contain dark internal laminae which often are stylolitic and comprise a complex mineralogy of muscovite, tourmaline, apatite, and rutile as well as containing pyrite, native gold and tellurides. So termed Group II ore bodies are located within steeply dipping ore bodies. In these, mineralisation is dominantly hosted within tectono – hydrothermal jig – saw breccia zones and veins. Breccia zones may be up to a few meters wide.</p> | <p>3.5 g/t Au but typically averages around 1 to 1.5 g/t Au.</p> <p>There is an indicated substantial hiatus between D<sub>2</sub> and D<sub>3</sub> and possibly D<sub>4</sub> stages. The latter (D<sub>3</sub>?) are characterised by an earlier pale to mid grey, aphanitic quartz + pyrite veinlets as a stockwork, crackle fill and hydrothermal jig – saw breccia styles within a zone of intense pervasive albitisation (30 to 60 vol%) alteration + disseminated pyrite mineralisation. This stage is overprinted by later stage of irregular stockwork type, milky white quartz + remnant chlorite veinlets ± disseminated pyrite attended by pervasive silicification and sericite + disseminated pyrite alteration. This may be a D<sub>4</sub> stage. A late pervasive style of pale glassy grey + fine grained arsenopyrite mineralisation replaces earlier mineralisation styles and is attended by roscoelite (V sericite) alteration.</p> |
| <p><b>Ore Body Geometry</b></p> | <p>Multiple ore-shoots in 20 defined ore bodies. These vary in their width and geologic strikes with widths varying from 2 to 10 meters.</p>  | <p>Multiple ore shoots are indicated with drill hole intercepts indicating shoots varying from 2 to 4 up to 6m in width.</p>   |